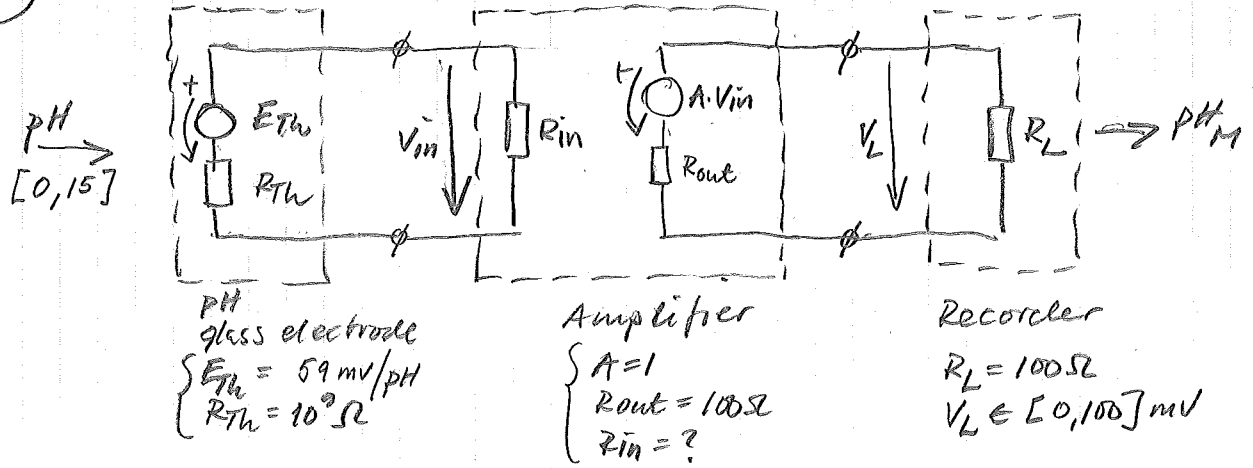
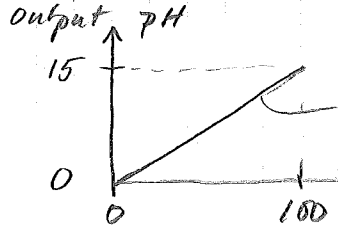


5.1



a) Sensitivity of the recorder scale K_R



$$\text{Slope } K_R = \frac{\Delta O}{\Delta E} = \frac{15}{100} = 0,15 \text{ pH/mV}$$

$$PH_M = V_L \cdot K_R$$

$$= A \cdot V_{in} \left(\frac{R_L}{R_L + R_{out}} \right) \cdot K_R$$

$$= A \cdot \left(E_{Th} \cdot \frac{R_{in}}{R_{in} + R_{Th}} \right) \left(\frac{R_L}{R_L + R_{out}} \right) \cdot K_R$$

$$= A \cdot (59 \cdot \text{pH}) \left(\frac{R_{in}}{R_{in} + R_{Th}} \right) \left(\frac{R_L}{R_L + R_{out}} \right) \cdot K_R$$

$$= A \cdot 59 \left(\frac{R_{in}}{R_{in} + R_{Th}} \right) \left(\frac{R_L}{R_L + R_{out}} \right) \cdot K_R \cdot \text{pH}$$

= 1 if no error

$$\Rightarrow K_R \cdot A \cdot 59 \left(\frac{R_{in}}{R_{in} + R_{Th}} \right) \left(\frac{R_L}{R_L + R_{out}} \right) = 1$$

$$= \frac{1}{2}$$

$$\frac{R_{in}}{R_{in} + R_{Th}} = \frac{2}{K_R \cdot A \cdot 59} = \frac{2}{0,15 \cdot 59}$$

$$2(R_{in} + 10^9) = 0,15 \cdot 59 \cdot R_{in}$$

$$R_{in}(0,15 \cdot 59 - 2) = 2 \cdot 10^9 \Rightarrow R_{in} = 2,92 \cdot 10^8 \Omega$$

5.1 cont.

b) $R_{Th} : 10^9 \Omega \quad \curvearrowright \quad 2 \cdot 10^9 \Omega$
 $pH = 7$

$$pH_M = 59 \cdot pH \left(\frac{R_{in}}{R_{in} + R_{Th}} \right) \cdot \left(\frac{R_L}{R_L + R_{out}} \right) \cdot K_R$$

$$= 59 \cdot 7 \cdot \underbrace{\left(\frac{2,92 \cdot 10^8}{2,92 \cdot 10^8 + 2 \cdot 10^9} \right)}_{= 0,1271} \cdot \underbrace{\left(\frac{100}{100 + 100} \right)}_{= \frac{1}{2}} \cdot 0,15 \approx 3,95$$

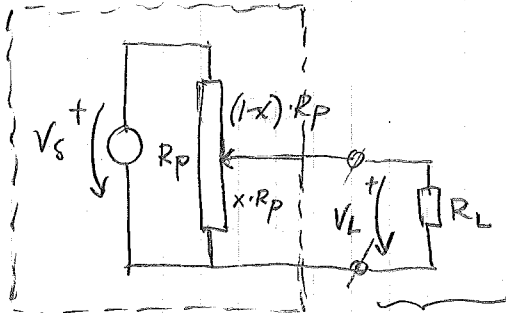
Error = $pH_M - pH = 3,95 - 7 = -3,05$

Percentage of full scale (= 15)

$$\frac{-3,05}{15} \cdot 100 = \underline{\underline{-20,3\%}}$$

5.2

The theory is presented in chapter 5.1.2
page 80-82.



Potentiometer displacement sensor

Recorder

• $R_L = 5000 \Omega$

• $l = 25 \text{ cm}$

• $P_{\text{max}} = 5 \text{ W}$

• $R_p \in [250, 2500] \Omega$
in steps of 250Ω

No loading: $V_{NL} = V_s \frac{x \cdot R_p}{R_p} = V_s \cdot x$ linear in x

Loading: $V_L = V_s \cdot x \cdot \frac{R_L}{R_p \cdot (1-x) + R_L}$ non-linear in x

page 81-82

$\Rightarrow N(x) = V_{NL} - V_L$

max non-linearity

if $R_p/R_L \ll 1$ $\hat{N} \approx 15 \cdot \frac{R_p}{R_L} \%$ of full span ($= V_s$)

$\hat{N} < 2\%$

$\Rightarrow 15 \cdot \frac{R_p}{R_L} < 2$

$R_p < \frac{2 \cdot R_L}{15} = \frac{2 \cdot 5000}{15} = 670 \Omega$

So $R_p < 670 \Omega$ due to non-linearity error

Select R_p !

$R_p < 670 \Omega$ and R_p in steps of 250Ω

$\Rightarrow R_p = 250 + 250 + \cancel{250}$

So R_p can be selected, according to

the requirements $\hat{N} < 2\%$; to 250Ω or 500Ω

5.2

cont.

- * Maximum sensitivity is achieved when V_s is as large as possible
- * But $P_{max} = 5W$ limit the possible value of V_s
- * $P = \frac{V_s^2}{R_p} \leq 5 (=P_{max})$ (*)

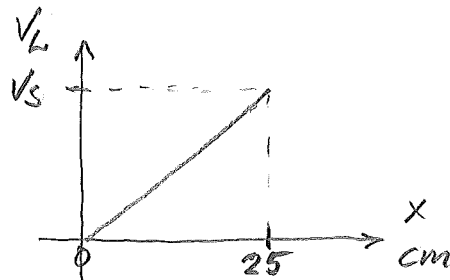
from (*): larger R_p gives higher V_s
 \Rightarrow select $R_p = 500 \Omega$

$$\text{So, } \frac{V_s^2}{500} \leq 5 \Rightarrow V_s \leq 50 \text{ V}$$

- b) Design for maximum sensitivity
 $\Rightarrow R_p = 500 \Omega$
 $V_s = 50 \text{ V}$

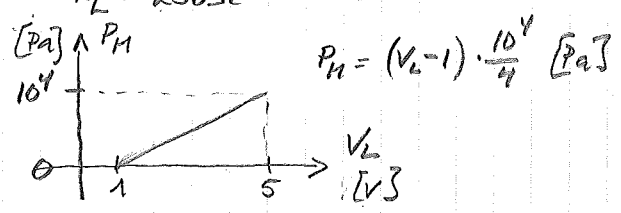
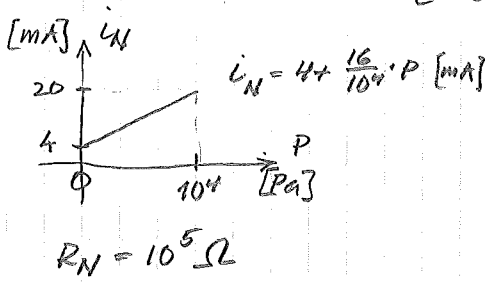
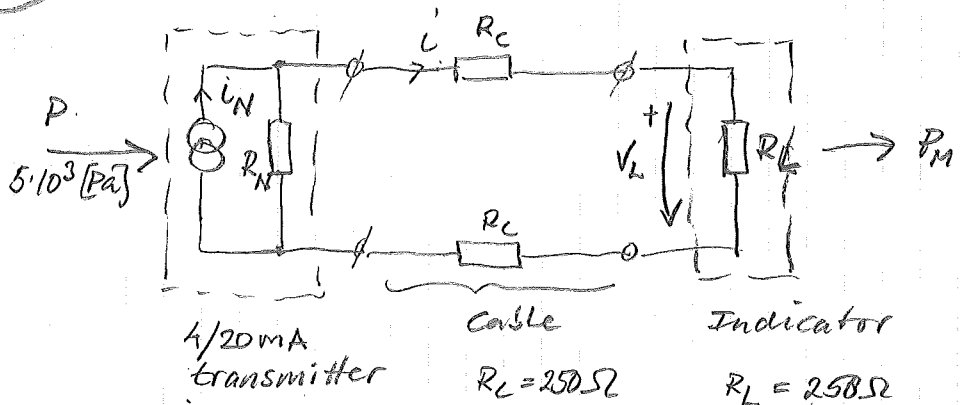
- a) Maximum sensitivity (unloaded sensor)
 V_L is linear in x

$$V_L = K \cdot x$$



$$K = \frac{V_s}{25} = \frac{50}{25} = 2 \text{ V/cm}$$

8.3



When input pressure $P = 5 \cdot 10^3$ [Pa] compute P_M .

$$i_N = 4 + \frac{16}{10^4} \cdot 5 \cdot 10^3 = 4 + 8 = 12 \text{ mA}$$

$$V_L = i \cdot R_L = \left(i_N \cdot \frac{R_N}{R_N + 2R_C + R_L} \right) \cdot R_L$$

$$= 12 \cdot 10^{-3} \left(\frac{10^5}{10^5 + 750} \right) \cdot 250 \approx 2,978 \text{ V}$$

$\approx 0,9926$

$$P_M = (V_L - 1) \frac{10^4}{4} = (2,978 - 1) \frac{10^4}{4} = 4,945 \cdot 10^3 \text{ [Pa]}$$

$$\text{Error} = P_M - P = (4,945 - 5) \cdot 10^3 = -0,055 \cdot 10^3$$

$$= -55 \text{ [Pa]}$$

Due to loading $i \neq i_N$
 less loading effect if $R_N \gg (2R_C + R_L)$
 No loading $\Rightarrow i = i_N$